Modelling, Design and Performance Analysis of LCL Filter for Grid Connected Three Phase Power Converters

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Authors’ contributions

This work was carried out in collaboration between both authors. Both authors read and approved the final manuscript.

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ABSTRACT

The use of Power Converters to integrate renewable sources of power with the ac grid has been on the increase in the last two decades. An LCL filter is often used to interconnect the Power Converters to the utility grid in order to filter the high order harmonics produced by the Converter. To achieve the high filtering performance that meet the stringent grid code requirement and also balance cost and effectiveness, an optimal design of the LCL filter is required. This paper presents the modelling and a comprehensive design methodology of an LCL filter for grid — interconnected converters using analytical approach. The simulation results show that with this design method, 99.51% of the current harmonics present at the converter output is mitigated.

Keywords: LCL filter; power converter; Total Harmonic Distortion (THD); passive damping.
ABBREVIATIONS

Currents

Ig : Grid Current  
lc  : Filter Capacitor Current

Voltages

Vg : Grid Voltage  
Vc : Voltage across Filter Capacitor  
Vin : Inverter voltage  
VB : Base Voltage  
VDC : DC Link Voltage

Inductances

L1 : Inverter Side Inductor  
L2 : Grid Side Inductor  
LB : Base Inductance

Resistances

R1 : Inverter Side Parasitic Resistance  
R2 : Grid Side Parasitic Resistance  
RD : Damping Resistor

Impedances

ZB : Base Impedance

Letters

S : Laplace transform operator  
F  : Frequency [Hz]  
L  : Inductor  
LC : Inductor Capacitor  
C  : Capacitor  
Fsw : Switching Frequency  
Fres : Resonance Frequency  
Pn : Rated Active Power  
En : Line to Line RMS Voltage

Greek letters

Ωres : Resonance Frequency of the LCL filter in radians/sec

Acronyms

MATLAB: Mathematics Laboratory  
AC : Alternating Current  
DC : Direct Current  
FFT : Fast Fourier Transform  
RES : Renewable Energy Sources  
Kw : Kilowatt  
EMI : Electromagnetic Interference  
IEC : International Electrotechnical Commission
1. INTRODUCTION

Use of Power Converters to interconnect to the grid has been on the increase in applications such as power quality, regenerative motor drive and distributed generation (DG) \[1\]. Various distributed generation systems like photo-voltaic (PV) and fuel cells produce energy in the form of DC voltage sources. Moreover, wind produces variable AC and is most times converted to DC also. Thus, when interfaced with a DC/AC inverter, these DG systems can supply energy into the utility grid. However, the power electronic devices used in these voltage source inverters (VSI), inject undesirable harmonics affecting the nearby loads at the point of common coupling (PCC) to the utility grid breaching the typical standards for grid interconnection.

Hence, to interface these power converters (VSI) to the utility grid, a filter is often required to reduce harmonics in the output current to desirable limits \[2\]. LCL-filter is among the best performing filters for grid-connected voltage source inverters (VSI), inject undesirable harmonics affecting the nearby loads at the point of common coupling (PCC) to the utility grid breaching the typical standards for grid interconnection.

Higher order LCL filters are essential to achieve these regulatory standard requirements at compact size and weight \[1\]. Designing of the LCL filter parameters (grid-side and inverter-side inductors and capacitor), takes an iterative approach due to the coherence between the filter parameters and these design requirements \[6\]. Because of these, typical design procedure for LCL filter is always complex. Therefore, the objective of this paper is to propose a simple design procedure for an LCL filter that meets Regulator’s requirement and to provide insight into methodologies for optimized filter design.

1.1 Advantage of High Order Filter Over First Order Filter

A simple first order L filter is not only bulky but fails to meet the stringent specifications for harmonic attenuation \[7\]. A third order LCL filter is now commonly used to achieve a higher attenuation \[8\] and standards with significant size and cost reduction of the components \[9,7\]. However designing an LCL filter systematically is a complex task \[6\]. Quite a number of important factors namely output current ripple, current harmonics sourced by insulated gate bipolar transistor (IGBT) switches, series fundamental drop, desirable power factor, resonance frequency, control stability are needed to be considered carefully \[9,7\]. Also, attention must be paid to the overall filter size and cost of its components while selecting various parameters for an efficient design. Fig. 6 gives a comparison between a first order (L) filter and a third order (LCL) filter.

2. CHARACTERIZATION OF HARMONICS IN PV INVERTER SYSTEM

The level and order of harmonics present in the output of a Voltage Source Inverter (VSI) is determined. The characterization is done to know the level of harmonics that is present in the output of a VSI.

Here, the Voltage Source Inverter (VSI) was implemented in a Simulink window and the output of the VSI is analyzed in terms of the harmonic content and distortion in the current waveform. Fig. 1 shows the Simulink model for the characterization.
2.1 Modeling and Design of LCL Filter

The transfer function model of the LCL filter is developed and the parameters of the model gotten through a clear design procedure. The modeling and the design of the LCL filter are done to determine the values of the parameters of the filter. The LCL filter is used to mitigate higher order harmonics present at the output of the VSI. A mathematical model is developed using the power circuit of a three phase grid connected VSI with LCL filter. The three phase power circuit is reduced to a single phase equivalent circuit and the transfer function of the LCL filter derived using the circuit parameters.

2.1.1 LCL filter mathematical model

The power circuit of a three phase grid connected power converter is presented in Fig. 2. As depicted in this figure and in the Single Phase equivalent circuit of Fig. 3, the LCL filter is used to interface between the grid and the power converter. V_g refers to the grid voltage, while L_1 and L_2 are the converter side inductor of the LCL filter and the grid side inductor of the LCL filter respectively. C refers to the LCL filter capacitor and R_D is the damping resistor. V_DC is the DC – Bus Voltage.

![Fig. 2. Power circuit of the three phase grid connected Inverter with LCL filter](image-url)
In the model of the LCL filter, we consider that;

- At frequencies other than the fundamental frequency, the grid behaves essentially as a short circuit, i.e. $V_g = 0$.

An important transfer function for the LCL filter is given as;

$$H = \frac{i_g}{V_{in}} = \frac{\text{Filter output current}}{\text{input voltage}} \quad (2.1)$$

Therefore, $H$ is an admittance transfer function and in the complex $S$ domain, we have;

$$H(s) = \frac{I_g(s)}{V_{in}(s)} \quad (2.2)$$

Applying Kirchhoff's laws, the equivalent circuit in Fig. 4, the mathematical model of the filter in s-plane is given by these equations:

$$I_{in} - I_c - I_g = 0 \quad (2.3)$$

$$V_{in} - V_c = I_{in} (sL_1 + R_1) \quad (2.4)$$

$$V_c - V_g = I_g (sL_2 + R_2) \quad (2.5)$$

$$V_c = I_c \left( \frac{1}{sC} + R_D \right) \quad (2.6)$$

The circuit parameters are defined as;

<table>
<thead>
<tr>
<th>Parameter</th>
<th>Description</th>
</tr>
</thead>
<tbody>
<tr>
<td>$V_{in}$</td>
<td>Inverter Voltage</td>
</tr>
<tr>
<td>$I_{in}$</td>
<td>Inverter Current</td>
</tr>
<tr>
<td>$V_c$</td>
<td>Voltage across Filter Capacitor</td>
</tr>
<tr>
<td>$I_c$</td>
<td>Filter Capacitor Current</td>
</tr>
<tr>
<td>$I_g$</td>
<td>Grid Current</td>
</tr>
<tr>
<td>$L_1$</td>
<td>Inverter side inductor</td>
</tr>
<tr>
<td>$L_2$</td>
<td>Grid side inductor</td>
</tr>
<tr>
<td>$C$</td>
<td>Capacitor</td>
</tr>
<tr>
<td>$R_D$</td>
<td>Damping Resistor</td>
</tr>
<tr>
<td>$V_g$</td>
<td>Grid voltage</td>
</tr>
<tr>
<td>$R_1$</td>
<td>Inverter Side Parasitic Resistance</td>
</tr>
<tr>
<td>$R_2$</td>
<td>Grid Side Parasitic Resistance</td>
</tr>
</tbody>
</table>

Fig. 4 gives the block diagram of the LCL Filter in the frequency domain.
Recall that for frequencies other than the fundamental frequency, $V_g = 0$.

Putting $V_g = 0$ in equation 2.5, gives:

$$V_c = I_g (sL_2 + R_2)$$

Equating 2.6 with 2.7 yields:

$$I_g (sL_2 + R_2) = I_c \left( \frac{1}{sC} + R_D \right)$$

This implies that:

$$I_c = I_g \left( \frac{s^2CL_2 + sCR_2}{sCR_D + 1} \right)$$

From equation 2.3,

$$I_{in} = I_c + I_g$$

Putting equation 2.9 into equation 2.10 gives:

$$I_{in} = I_g + I_g \left( \frac{s^2CL_2 + sCR_2}{sCR_D + 1} \right)$$

Also, from equation 2.4,

$$V_{in} = V_c + I_{in} (sL_1 + R_1)$$

Substituting equations 2.7 and 2.11 into 2.12 gives:

$$V_{in} = I_g (sL_2 + R_2) + (sL_1 + R_1) \left( I_g + I_g \left( \frac{s^2CL_2 + sCR_2}{sCR_D + 1} \right) \right)$$

$$V_{in} = I_g \left( (sL_1 + R_1) + (sL_2 + R_2) + \frac{(sL_1 + R_1)(s^2CL_2 + sCR_2)}{sCR_D + 1} \right)$$
\[ V_{in} = I_g \left[ s^3 C L_1 L_2 + s^2 C (L_1 (R_2 + R_D) + L_2 (R_1 + R_D)) + s(L_1 + L_2 + C (R_1 R_2 + R_1 R_D + R_2 R_D)) \right] + \frac{R_1 + R_2}{sCR_D + 1} \]

Therefore, the transfer function according to equation 2.2 is:

\[ H_{dLCL}(s) = \frac{sCR_D + 1}{s^3 C L_1 L_2 + s^2 C (L_1 (R_2 + R_D) + L_2 (R_1 + R_D)) + s(L_1 + L_2 + C (R_1 R_2 + R_1 R_D + R_2 R_D)) + R_1 + R_2} \] (2.16)

Without the damping resistance \( R_D \), equation 2.16 becomes:

\[ H_{LCL}(s) = \frac{1}{s^3 C L_1 L_2 + s^2 C (L_1 R_2 + L_2 R_1) + s(L_1 + L_2 + C (R_1 R_D) + R_1 + R_2} \]

The effect of the damping resistor is seen in the frequency plots of Fig. 7.

2.2 LCL Filter Design Procedure

The LCL filter design methodology is aimed to meet grid code requirements through efficient attenuation of high order current harmonic components on the grid side. It requires the following nominal system parameters. Table 1 shows the nominal system parameters used in the design.

**Base Values:**

Base voltage \( V_B = E_n = \sqrt{3} \times V_g = \sqrt{3} \times 240 = 415V \)

Base Impedance \( Z_B = \frac{E_n^2}{P_n} = \frac{415^2}{100000} = 1.7223\Omega \)

Base angular frequency \( \omega_g = 2\pi f_g = 2\pi \times 50 = 314.2\ text{rads} \)

Base Capacitance \( C_B = \frac{1}{\omega g Z_B} = \frac{1}{314.2 \times 1.7223} = 1847.93\mu\text{F} \)

Base Inductance \( L_B = \frac{Z_B}{\omega_g} = \frac{1.7223}{314.2} = 5.482\text{mH} \)

Any quantity when divided by its base value is expressed in p.u. (per unit) Important Ratios:

- Ratio between the LCL filter inductances, otherwise called split factor

\[ r_1 = \frac{L_2}{L_1} \] (2.18)

- Ratio between the LCL filter capacitance and total inductance in p.u.

\[ r_q = \frac{C}{L_T} = \frac{Z_B^2 C}{L_T} \] (2.19)
• Ratio between the switching and resonance frequency

$$\frac{r_f}{f_{res}} = \frac{\omega_{sw}}{\omega_{res}}$$  \hspace{1cm} (2.20)

2.2.1 LCL filter design criteria

The following are some important design criteria for the LCL filter.

- Fulfillment of reactive volt-ampere (VAR) limits (power factor nearly equal to 1)
- Optimal volume and weight with resulting minimum cost of passive (inductive and capacitive) components
- Attenuation of higher order harmonics from the output current (THD≤ 0.03)
- Proper choice of resonance frequency such that the switching harmonics are sufficiently attenuated and the size of the filter components is not too large \([2, 8, 10]\) \((10f_g \leq f_{res} \leq 0.5f_{sw})\).

2.2.2 Inverter side inductance design

For the first step, we have to design the inverter side inductance. To do this, the approach propose by \([11, 12]\) is adopted.

Here, we consider the maximum current ripple present at the output of an inverter which is given as;

$$\Delta I_{L_{max}} = \frac{2V_{DC}}{3L_1} \left(1 - m\right) m T_{sw}$$ \hspace{1cm} (2.21)

Equation 2.21 appears as equation (13) in Reznik et al. \([11]\) and as equation (5) in Yitao et al. \([12]\).

Where \(m\) is modulation index and \(T_{sw} = \frac{1}{f_{sw}}\).

But, maximum peak to peak current ripple occurs when \(m\) is 0.5. Thus, equation 2.21 becomes;

$$\Delta I_{L_{max}} = \frac{V_{DC}}{6f_{sw} L_1}$$ \hspace{1cm} (2.22)

Considering a 10% ripple of the rated current for the design parameters, equation 2.21 is given by:

$$\Delta I_{L_{max}} = 0.1 I_{max}$$ \hspace{1cm} (2.23)

Where;

$$I_{max} = \frac{\sqrt{2} P_n}{3V_{ph}}$$ \hspace{1cm} (2.24)

$$L_1 = \frac{V_{DC}}{6f_{sw} \Delta I_{L_{max}}}$$ \hspace{1cm} (2.25)

From equation 2.25, we have;

$$L_1 = \frac{800}{6 \times 16000 \times 19.64} = 0.424 mH$$
2.2.3 Maximum LCL filter capacitor value

A lesser value of the filter capacitor $C$ will reduce unnecessary flow of larger reactive currents through it. We know that the flow of reactive power is tied to voltage stability. Therefore, a larger value of $C$ can introduce voltage instability problems in the grid. In this case, the LCL filter capacitor $C$ is designed so that its consumption of reactive power is less than $n\%$ of the rated power $P_n$ as shown in Equation (2.26a) [10]. In this equation, $Q_c$ denotes the reactive power consumed by the filter capacitor and $n$ is a positive factor chosen and is generally equal to or less than 5% [2,10]. According to Equations (2.26a) and (2.26b), the maximum value of the filter capacitor can be expressed as in Equation (2.26c):

$$Q_c = n\%P_n$$  \hspace{1cm} 2.26a

But,

$$Q_c = -E_n^2C\omega_g$$  \hspace{1cm} 2.26b

This implies that for $n = 5\%$,

$$C_{max} = 0.05\left(\frac{P_n}{3V_g^2\omega_g}\right)$$  \hspace{1cm} 2.26c

$$C_{max} = 92.4\mu F$$

In this case, $C = C_{max}$ and is exactly 5\% of the base capacitance $C_B$.

Equation 2.26a appears as equation (14a) in Ben Said-Romdhane et al. [10].

2.2.4 Grid side inductance design

To obtain a ripple attenuation of 20\% on the grid side with respect to the current ripple on the inverter side,

$$L_2 = \frac{1}{\sqrt{k^2 + 1}} \frac{1}{Cf_{sw}^2}$$  \hspace{1cm} (2.27)

The attenuation factor $k$ in equation 2.27 is set to a value of 20\% (0.2).

$$L_2 = \sqrt{\frac{1}{0.2^2} + 1} \frac{1}{92.4 \times 10^{-6} \times 16000^2} = 0.254 mH$$

2.2.5 Resonance frequency design

The resonance frequency depends on the filter inductors $L_1$ and $L_2$ and the filter capacitor $C$.

Let $L = L_1 + L_2$ and $L_p = \frac{L_1L_2}{L_1+L_2}$

But generally for any given tank circuit, $\omega_{res} = \frac{1}{\sqrt{L_p}}$

Thus, for the LCL filter,
\[
\omega_{res} = \frac{1}{\sqrt{L_p C}}
\]  
(2.28)

Also, the calculated value of \(\omega_{res}\) must satisfy the inequality given in equation 2.29. Otherwise, the values of equation 2.27 is re-chosen.

\[
10f_g \leq f_{res} \leq 0.5f_{sw}
\]  
(2.29)

Note that \(\omega_{res}\) is in radians.

From equation 2.28:

\[
\omega_{res} = \frac{1}{\sqrt{0.000158843 \times 92.4 \times 10^{-6}}} = 8254.29 \text{ rads/sec}
\]

\[
f_{res} = \frac{8254.29}{2\pi} = 1313.71 \text{ Hz}
\]

In this case, \(f_{res}\) is taken to be 1500Hz (i.e. \(w_{res} = 9425 \text{ rads/sec}\)) and this satisfies the inequality in equation 2.29.

### 2.2.6 Minimum DC bus voltage

According to Ben Said-Romdhane et al. [10]. For Voltage source converter, the DC-bus voltage will decide the maximum AC voltage that can be generated. A general guideline will be that the minimum DC voltage should be equal to the maximum line-to-line voltage of the grid. For three-phase grid, this will be the peak value of the line-to-line voltage.

Thus,

\[
V_{DC_{min}} = \sqrt{2} V_L
\]  
(2.30)

\(V_L\) is the line-to-line voltage of the grid.

\[
V_{DC_{min}} = 587\text{V}
\]

In this design, \(V_{DC}\) is 800V.

### 2.2.7 Damping resistor design

For this design, we consider a simple passive damping where a resistor \(R_D\) is inserted in series with the capacitor to attenuate part of the ripple on the switching frequency in order to avoid resonance. According to Reznik et al. [11], the value of this resistor should be one third of the impedance of the filter capacitor at the resonance frequency. That is:

\[
R_D = \frac{1}{3\omega_{res} C}
\]  
(2.31)

\[
R_D = \frac{1}{3 \times 238.73 \times 92.4 \times 10^{-6}} = 15\Omega
\]

Equation 2.31 appears as equation (23) in Reznik et al. [11].

But Pena-Alzola et al. [13], gives an expression for the minimum damping resistor \(R_{D_{min}}\). The authors revealed that for the system to be stable and in order to achieve a positive gain margin in the control of the system, the damping resistor value must comply with equation 2.32.
\[ R_{D_{\text{min}}} = \frac{1}{3} f_{sw} \left( \frac{L_2^2}{L_1 + L_2} \right) \]  

Equation 2.32 appears as equation (5) in Pena-Alzola et al. [13].

This means that the choice of \( R_D \) should be such that it satisfies the relation; 
\[ 0.51 \leq R_D \leq 15 \]

Note: \( R_1 \) and \( R_2 \) are parasitic resistances of the inductors \( L_1 \) and \( L_2 \) respectively and their values can be chosen directly from the manufacturer’s datasheet. In this case; \( R_1 = 0.380 \Omega \) and \( R_2 = 0.162 \Omega \). Table 1 shows the design system parameters that will be used for the simulation.

2.2.8 Simulink model of the inverter system with the LCL filter

Figure 5 shows the Simulink model of the Inverter system with the LCL filter. Here, the design parameters as shown in Table 1 was used to develop a Simulink model to carry out performance analysis on the LCL filter.

3. RESULTS AND DISCUSSION

3.1 Comparison of Harmonic Attenuation of LCL and L Filters

Fig. 6 gives Bode plots comparing the attenuation capabilities of LCL and L filters. It shows that a third order (LCL) filter is superior at attenuating higher harmonic frequencies and can therefore be designed to meet the stringent specifications for harmonic attenuation. This is because for the same (or lower) net inductance \((L_1+L_2)\) we have better attenuation \((60\text{ dB/decade})\) in third order filter at frequencies above the resonance frequency as against \(20\text{ dB/decade}\) obtained with the first order (L) filter.

3.2 Frequency Plots for Damped and Undamped LCL Filter

The Bode plots of the LCL filter without and with damping are shown in Fig. 7. The insertion of a series resistance with the capacitor eliminates the gain spike, smoothing the overall response and rolling-off to \(-180\) degrees for high frequency, instead of \(-270\) degrees. The LCL filter can achieve high performance at high frequency with an attenuation rate of \(-60\text{ dB/decade}\).
3.3 Harmonics in the PV Inverter System

In this section, the harmonic content in the unfiltered PV inverter system is presented. The current waveform and the Fast Fourier Transform (FFT) analysis are considered. From Fig. 8, it is seen that the current waveform is actually far from being sinusoidal due to very high content of harmonics. Fig. 9 gives the FFT analysis of this system, the Total Harmonic Distortion (THD) is as high as 85.62%, making it impossible and unsuitable for grid connected application. Utility operators accept a THD of less than 5% for all grid connected systems.
Fig. 8. Current waveform of the PV Inverter System

Fundamental (50Hz) = 128.8, THD = 85.62%

Fig. 9. FFT analysis of the PV Inverter System

Table 1. Design System Parameters

<table>
<thead>
<tr>
<th>Symbol</th>
<th>Description</th>
<th>Value</th>
</tr>
</thead>
<tbody>
<tr>
<td>( f_g )</td>
<td>Grid frequency or fundamental frequency</td>
<td>50Hz</td>
</tr>
<tr>
<td>( f_{sw} )</td>
<td>PWM carrier frequency</td>
<td>16KHz</td>
</tr>
<tr>
<td>( W_{res} )</td>
<td>Resonance frequency</td>
<td>9425 rads/sec</td>
</tr>
<tr>
<td>( P_n )</td>
<td>Rated active power</td>
<td>100KW</td>
</tr>
<tr>
<td>( E_n )</td>
<td>Line to line RMS voltage</td>
<td>( \sqrt{3} \times 240 ) V</td>
</tr>
<tr>
<td>( V_{DC} )</td>
<td>DC Bus voltage</td>
<td>800V</td>
</tr>
<tr>
<td>( L_1 )</td>
<td>Inverter side inductor</td>
<td>0.424mH</td>
</tr>
<tr>
<td>( L_2 )</td>
<td>Grid side inductor</td>
<td>0.254mH</td>
</tr>
<tr>
<td>( R_1 )</td>
<td>Inverter Side Parasitic Resistance</td>
<td>0.380 ( \Omega )</td>
</tr>
<tr>
<td>( R_2 )</td>
<td>Grid Side Parasitic Resistance</td>
<td>0.162 ( \Omega )</td>
</tr>
<tr>
<td>( C )</td>
<td>Capacitor</td>
<td>92.4( \mu )F</td>
</tr>
<tr>
<td>( R_D )</td>
<td>Damping Resistor</td>
<td>2.2( \Omega )</td>
</tr>
<tr>
<td>( V_g )</td>
<td>Grid voltage</td>
<td>240V</td>
</tr>
</tbody>
</table>
3.4 The PV Inverter System Simulation Parameters

The inverter system is simulated using the design parameters obtained in section 2. The nominal system parameters and the design parameters are given in Table 1.

3.5 Simulation Results of the LCL Filter

Fig. 10 shows the output current waveform of the inverter system with the LCL filter. Here, it is seen that the waveforms are all sinusoidal at this point since a greater percentage of the harmonics present at the output of the PV inverter system has been filtered out by the well-designed LCL filter. The harmonic content has also been reduced from 85.62% to 0.42%. However, Fig. 11 reveals that the LCL filter cannot optimally handle the low order harmonics, hence the need for a current controller. The current controller is needed to filter out the low order harmonics to make the PV inverter system meet utility ‘Standard for Interconnecting Distributed Resources with Electric Power Systems’. To achieve smooth integration of renewable energy sources into the grid, a current

![Fig. 10. Three – phase Output Current Waveforms with LCL Filter](image)

![Fig. 11. FFT analysis of the PV Inverter System with LCL filter](image)
controller will be incorporated into the system. Current control techniques help inverters to provide stability, low steady state error, fast transient response and low total harmonic distortion.

4. CONCLUSION

This paper proposes a simple, robust and systematic design methodology for an LCL filter, used to interface between three phase power converter and the utility grid. This filter is used to reduce the switching frequency current harmonics produced by the power converter. The proposed design methodology is simple, efficient and aimed to meet the grid code requirements. Compared to classical design methodologies, the proposed method is simple and straightforward. Moreover, it takes into account four paramount design criteria - fulfillment of reactive volt-ampere (VAR) limits, optimal volume of the filter, THD ≤ 0.003 and proper choice of resonance frequency. The obtained filter parameters were tested using MATLAB-Simulink software tool. The obtained simulation results show the reliability, efficiency and high filtering performances of the proposed design methodology. The simulation results show that with this design method, over 99.51% of the current harmonics present at the converter output is mitigated.

IEEE Standard 519 establishes harmonic limits as 5% for total harmonic distortion (THD). Therefore, the proposed design methodology meets industrial standard. This study therefore can be deployed for large scale smooth integration of renewable energy sources into the grid.

COMPETING INTERESTS

Authors have declared that no competing interests exist.

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